

# Capacitance of Coupled Circular Microstrip Disks

MASARU TAKAHASHI AND KOHEI HONGO, SENIOR MEMBER, IEEE

**Abstract**—The coupling between circular disks placed on a grounded dielectric substrate is studied analytically and numerically. The problem is formulated exactly by applying the Kobayashi potential, which uses discontinuity properties of Weber–Schafheitlin integrals, as an electrostatic problem when the potentials on the disks are specified. Numerical results for charge distribution and gap capacitance are presented. The potential distribution on the disks is calculated numerically to check if it satisfies the specified boundary condition.

## I. INTRODUCTION

THE ELECTROSTATIC problem of a pair of identical circular disk condensers has claimed the attention of numerous investigators over a long span of time [1]–[4]. Approximate solutions of this problem have been derived by Kirchhoff, who refers to earlier papers by Clausius and Helmholtz and improves the previous crude estimate for capacitance by suggesting a plausible edge correction (also, see papers by Maxwell, Ignatowsky, Polya and Szego, and others [1], [2]). An exact solution of this problem also has been attacked, and we can refer to papers by Love, Nicholson [1], and Nomura [3]. A critical review of the approximate solutions has been given by Hutson [2], using Love's integral equation, and by Leppington and Levine [4], using another integral equation.

Recently, the fringing effects on the capacitance of a circular parallel-plate capacitor filled with dielectric has become an important topic because it has application to microstrip circuits [5], [6]. The problem can be formulated rigorously by applying a dual integral equation [5], [6] or applying the Kobayashi potential [7], the name given by Sneddon [1] to the expression for the potential constructed by using the properties of Weber–Schafheitlin integrals proposed by Kobayashi in 1931. For practical purposes the coupling between printed microstrip circuit components is an important problem [8], [9]. As is pointed out by Sneddon, the problem of determining the electrostatic potential of the field due to two equal coplaner electrified disks is a difficult one, so that the problems have been little studied since Kobayashi [10] showed one of the approaches to those kinds of problems. Recently, Uzunoglu and Katechi [11] studied the more general problem of a coupled microstrip resonator using numerical methods and obtained some numerical results for gap capacitance. Their

study concentrates on determining a resonant frequency. It is the purpose of this paper to treat this problem rigorously as an electrostatic potential problem and to obtain numerical results for a wider range of physical quantities such as potential distribution and charge distribution, as well as gap capacitance. We followed Kobayashi's procedure as an analytical method. The obtained numerical information will serve as a confirmation of the newly developed analytical technique as well as for the practical design of microwave integrated circuits. To check the validity of the present treatment we compared the calculated potential on the disks with specified values, and agreement between them is satisfactory for practical purposes.

## II. STATEMENT OF THE PROBLEM

The geometry of the problem is depicted in Fig. 1. Circular disks of the same size are placed on a grounded dielectric substrate. The thickness and relative dielectric constant of the substrate are  $h$  and  $\epsilon_r$ , respectively. The separation between the centers of the disks is  $pa$ , where  $a$  is radius of the disk. We will consider the case when potential distributions of the disks are specified as  $f_1(r_1, \theta_1)$  and  $f_2(r_2, \theta_2)$ , where  $(r_1, \theta_1)$  and  $(r_2, \theta_2)$  are local cylindrical coordinates whose origins are located at the centers of disk 1 and disk 2, respectively. According to the method of the Kobayashi potential, we can assume a potential function in each region as follows:

$$\begin{aligned} \Phi_1^{(1)} = & \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(1)} \cos m\theta_1 \\ & + B_{mn}^{(1)} \sin m\theta_1) W_1(\rho_1, z) \\ \Phi_1^{(2)} = & \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(2)} \cos m\theta_2 \\ & + B_{mn}^{(2)} \sin m\theta_2) W_1(\rho_2, z) \quad (z \geq h) \quad (1) \end{aligned}$$

$$\begin{aligned} \Phi_2^{(1)} = & \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(1)} \cos m\theta_1 \\ & + B_{mn}^{(1)} \sin m\theta_1) W_2(\rho_1, z) \\ \Phi_2^{(2)} = & \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(2)} \cos m\theta_2 \\ & + B_{mn}^{(2)} \sin m\theta_2) W_2(\rho_2, z) \quad (h \geq z \geq 0) \quad (2) \end{aligned}$$

where  $\rho_1 = r_1/a$ ,  $\rho_2 = r_2/a$  and,  $W_1(\rho, z)$  and  $W_2(\rho, z)$  are

Manuscript received April 7, 1982; revised June 14, 1982.

The authors are with the Faculty of Engineering, Shizuoka University, Hamamatsu, 432, Japan.

defined by

$$W_1(\rho_i, z) = \int_0^\infty \frac{J_m(\rho_i \xi) J_{m+2n+1/2}(\xi)}{\sqrt{\xi}} f_i(\xi) \cdot \exp \left[ -\frac{z-h}{a} \xi \right] d\xi$$

$$W_2(\rho_i, z) = \int_0^\infty \frac{J_m(\rho_i \xi) J_{m+2n+1/2}(\xi)}{\sqrt{\xi}} g_i(\xi) \cdot \sinh \left( \frac{z}{a} \xi \right) d\xi \quad (i=1,2) \quad (3)$$

where  $f_i(\xi)$  and  $g_i(\xi)$  ( $i=1,2$ ) are unknown functions which are to be determined so that the potential function defined in (2) satisfies the boundary conditions on the surface of the substrate except the conducting disks. In the above equations,  $\Phi_1^{(1)}$  and  $\Phi_2^{(1)}$  are potential functions when disk 2 is absent, while the function  $\Phi_1^{(2)}$  and  $\Phi_2^{(2)}$  are those when disk 1 is absent. Imposing the continuity of potential functions and electric flux on the surface of the dielectric substrate, the potential functions of the problem given in Fig. 1 may be expressed as

$$\Phi_1 = \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(1)} \cos m\theta_1 + B_{mn}^{(1)} \sin m\theta_1) U_1(\rho_1, z)$$

$$+ \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(2)} \cos m\theta_2 + B_{mn}^{(2)} \sin m\theta_2) U_1(\rho_2, z) \quad (z \geq h) \quad (4a)$$

$$\Phi_2 = \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(1)} \cos m\theta_1 + B_{mn}^{(1)} \sin m\theta_1) U_2(\rho_1, z)$$

$$+ \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} (A_{mn}^{(2)} \cos m\theta_2 + B_{mn}^{(2)} \sin m\theta_2) U_2(\rho_2, z) \quad (0 \leq z \leq h) \quad (4b)$$

$$U_1(\rho_i, z) = \int_0^\infty \frac{J_m(\rho_i z) J_{m+2n+1/2}(\xi)}{\sqrt{\xi}} P(\xi, h) \cdot \exp \left[ -\frac{z-h}{a} \xi \right] d\xi$$

$$U_2(\rho_i, z) = \int_0^\infty \frac{J_m(\rho_i \xi) J_{m+2n+1/2}(\xi)}{\sqrt{\xi}} P(\xi, z) d\xi$$

$$P(\xi, z) = \frac{\sinh \left( \frac{z}{a} \xi \right)}{\epsilon_r \cosh \left( \frac{h}{a} \xi \right) + \sinh \left( \frac{h}{a} \xi \right)} \quad (i=1,2). \quad (4c)$$

The expansion coefficients  $A_{mn}$  and  $B_{mn}$  are to be determined so that  $\Phi_1$  and  $\Phi_2$  reduce to specified potential distributions  $f_1(r_2, \theta_1)$  and  $f_2(r_2, \theta_2)$  on the disks. Though  $\Phi_1$  and  $\Phi_2$  in (3) give a general solution when arbitrary potential distributions are specified on each disk, we will restrict ourselves at this stage to the special case of a

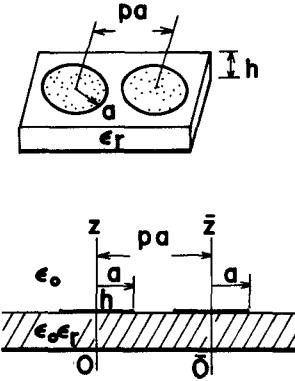


Fig. 1. Geometry of the problem.

constant potential on the disk, since the conducting disk is at an equipotential in practical situations. Since the expressions for  $\Phi_1$  and  $\Phi_2$  are mixed functions of variables  $(r_1, \theta_1)$  and  $(r_2, \theta_2)$ , they must be transformed to the function of only  $(r_1, \theta_1)$  or  $(r_2, \theta_2)$  when we impose the boundary condition on each disk. This is realized by applying the addition theorem of Bessel functions. Setting  $\Phi_{1,2}|_{z=h} = V_1$ ,  $(0 < r_1 < a, 0 < \theta_1 < 2\pi)$ ,  $\Phi_{1,2}|_{z=h} = V_2$ ,  $(0 < r_2 < a, 0 < \theta_2 < 2\pi)$ , and using properties of the Fourier series, we obtain the following relations:

$$\sqrt{\frac{2}{\pi}} \sum_{n=0}^{\infty} \left[ A_{0n}^{(i)} \int_0^\infty \frac{J_0(\rho_i \xi) J_{2n+1/2}(\xi)}{\sqrt{\xi}} P(\xi, h) d\xi \right. \\ \left. + \sum_{m=0}^{\infty} A_{mn}^{(j)} \int_0^\infty \frac{J_0(\rho_i \xi) J_m(p \xi) J_{m+2n+1/2}(\xi)}{\sqrt{\xi}} P(\xi, h) d\xi \right] = V_i \quad (5a)$$

$$\sqrt{\frac{2}{\pi}} \sum_{n=0}^{\infty} \left[ A_{ln}^{(i)} \int_0^\infty \frac{J_l(\rho_i \xi) J_{l+2n+1/2}(\xi)}{\sqrt{\xi}} P(\xi, h) d\xi \right. \\ \left. + \sum_{m=0}^{\infty} A_{mn}^{(j)} \int_0^\infty \frac{J_l(\rho_i \xi) J_{l+2n+1/2}(\xi)}{\sqrt{\xi}} P(\xi, h) d\xi \right. \\ \left. \cdot \{ J_{l+m}(p \xi) + (-1)^l J_{l-m}(p \xi) \} d\xi \right] = 0 \quad (5b)$$

where  $j = 2/i$ , ( $i=1,2$ ). Expanding the Bessel functions  $J_m(\rho_i \xi)$  in (5) by Jacobi's polynomials  $u_n^m(\rho^2)$  as defined in the Appendix, and using the orthogonality of the polynomials, we derive determinantal equations for expansion coefficients  $A_{mn}$ . The results are expressed as

$$\sum_{n=0}^{\infty} A_{0n}^{(i)} G A(0, n, k) + \sum_{n=0}^{\infty} \sum_{m=0}^{\infty} A_{mn}^{(j)} H(0, m, n, k) = C_i^{(i)}$$

$$\sum_{n=0}^{\infty} A_{ln}^{(i)} G A(l, n, k) + \sum_{n=0}^{\infty} \sum_{m=0}^{\infty} A_{mn}^{(j)} H(l, m, n, k) = 0$$

$$(l=1,2,\dots, \quad k=0,1,2,\dots) \quad (6)$$

where

$$\begin{aligned} GA(l, n, k) &= \int_0^\infty \frac{J_{l+2n+1/2}(\xi) J_{2k+1/2}(\xi)}{\xi} P(\xi, h) d\xi \\ H(l, n, m, k) &= \frac{1}{1 + \delta_{0l}} \int_0^\infty \frac{J_{m+2n+1/2}(\xi) J_{l+2k+1/2}(\xi)}{\xi} \\ &\quad \cdot P(\xi, h) \{ J_{m+l}(p\xi) + (-1)^l J_{m-l}(p\xi) \} d\xi \\ C_k^{(i)} &= V_i \delta_{k0}, \quad j = 2/i \quad (i = 1, 2). \end{aligned} \quad (7)$$

Once the expansion coefficients  $A_{mn}$  are determined from (6) the potential at any points is calculated from

$$\begin{aligned} \begin{pmatrix} \Phi_1 \\ \Phi_2 \end{pmatrix} &= \sqrt{\frac{2}{\pi}} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} \left\{ A_{mn}^{(1)} \begin{pmatrix} U_1(\rho_1, z) \\ U_2(\rho_1, z) \end{pmatrix} \cos m\theta_1 \right. \\ &\quad \left. + A_{mn}^{(2)} \begin{pmatrix} U_1(\rho_2, z) \\ U_2(\rho_2, z) \end{pmatrix} \cos m\theta_2 \right\} \end{aligned} \quad (8)$$

where functions  $U(\rho, z)$  are defined in (4c). The expressions for charge distribution  $\sigma_1$  and  $\sigma_2$  on the surface of disk 1 and disk 2, respectively, are derived from  $\Phi_1$  and  $\Phi_2$ . The expressions for  $\sigma_1$  and  $\sigma_2$  are given by

$$\begin{aligned} \sigma_i(\rho_i, \theta) &= -\epsilon_0 \left\{ \frac{\partial \Phi_1}{\partial z} \Big|_{z=h} - \epsilon_r \frac{\partial \Phi_2}{\partial z} \Big|_{z=h} \right\} \\ &= \sqrt{\frac{2}{\pi}} \frac{\epsilon_0}{a} \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} A_{mn}^{(i)} \cos m\theta_i \\ &\quad \cdot \int_0^\infty \sqrt{\xi} J_m(\rho_i \xi) J_{m+2n+1/2}(\xi) d\xi \quad (i = 1, 2). \end{aligned} \quad (9)$$

The charge density outside of the disk on the surface of the substrate is found to be zero since the above integral is shown to vanish for  $\rho_i > 1$  using the properties of Weber–Schafheitlin’s integral [12]. For  $0 < \rho_i < 1$ , the integral can be expressed in terms of a hypergeometric series. The result is

$$\begin{aligned} \int_0^\infty \sqrt{\xi} J_m(\rho_i \xi) J_{m+2n+1/2}(\xi) d\xi &= \frac{\sqrt{2} \Gamma(m+n+1) \rho^m}{\Gamma(m+1) \Gamma(n+1/2)} \\ &\quad \cdot F\left(m+n+1, \frac{1}{2} - n, m+1, \rho^2\right) \\ &= \frac{\sqrt{2} \Gamma(m+n+1)}{\Gamma(m+1) \Gamma(n+1/2)} \frac{\rho^m}{\sqrt{1-\rho^2}} F \\ &\quad \cdot \left(-n, m+n+\frac{1}{2}, m+1, \rho^2\right) \end{aligned} \quad (10)$$

where the relation  $F(a, b, c; z) = (1-z)^{c-a-b} F(c-a, c-b, c; z)$  is used to derive the second expression on the right-hand side of the above equation, which is a polynomial of order  $n$ . The total charge on the disk is obtained by integrating the charge density over the disk. The total

charge of disk 1 is given by

$$\begin{aligned} Q_1 &= a^2 \int_0^{2\pi} d\theta_1 \int_0^1 \rho_1 d\rho_1 \sigma_1(\rho_1, \theta_1) \\ &= 2\sqrt{2\pi} a \epsilon_0 \sum_{n=0}^{\infty} A_{0n}^{(1)} \int_0^\infty \sqrt{\xi} J_{2n+1/2}(\xi) d\xi \\ &\quad \cdot \int_0^1 J_0(\rho_1 \xi) \rho_1 d\rho_1 \\ &= 2\sqrt{2\pi} a \epsilon_0 \sum_{n=0}^{\infty} A_{0n}^{(1)} \int_0^\infty \frac{J_1(\xi) J_{2n+1/2}(\xi)}{\sqrt{\xi}} d\xi \\ &= 4a\epsilon_0 A_{00}^{(1)} \end{aligned} \quad (11)$$

where we used the formula [12]

$$\int_0^1 \frac{J_1(\xi) J_{2n+1/2}(\xi)}{\sqrt{\xi}} d\xi = \sqrt{\frac{2}{\pi}} \delta_{0n}. \quad (12)$$

Similarly, the total charge of disk 2 is expressed as  $Q_2 = 4a\epsilon_0 A_{00}^{(2)}$ .

### III. NUMERICAL RESULTS AND DISCUSSION

In this section we present some numerical results for physical quantities. Firstly, we have determined the numerical value of the function  $GA$  and  $H$  defined in (7) to obtain a solution for  $A_{mn}$  from (6). Since it is difficult to calculate the integrals  $GA$  and  $H$  analytically, we get the results by numerical integration.  $GA$  and  $H$  are written as

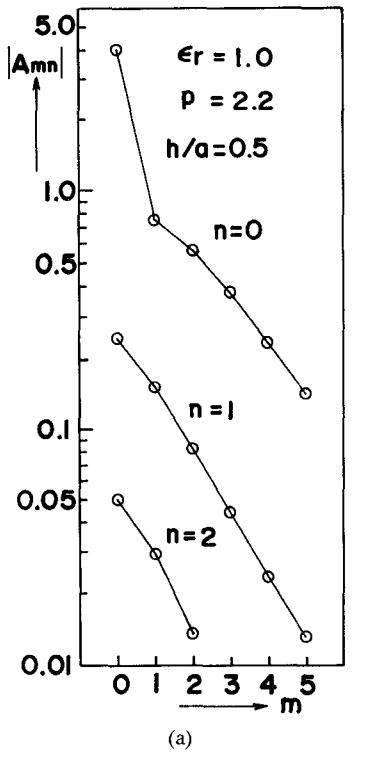
$$\begin{aligned} GA(n, k) &= \int_0^\infty \frac{J_{2n+1/2}(\xi) J_{2k+1/2}(\xi)}{\xi} \\ &\quad \cdot \left\{ P(\xi, h) - \frac{1}{\epsilon_r + 1} \right\} d\xi + GA_0(n, k) \end{aligned} \quad (13a)$$

$$\begin{aligned} H(n, m, k) &= \int_0^\infty \frac{J_{2n+m+1/2}(\xi) J_{2k+1/2}(\xi) J_m(\rho\xi)}{\xi} \\ &\quad \cdot \left\{ P(\xi, h) - \frac{1}{\epsilon_r + 1} \right\} d\xi + H_0(n, m, k) \end{aligned} \quad (13b)$$

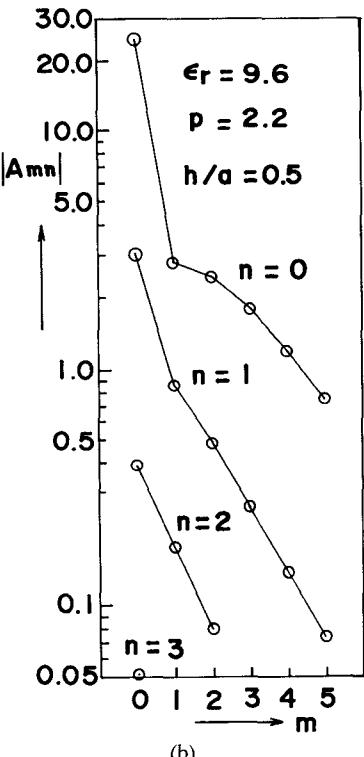
where the integrals  $GA_0(n, k)$  and  $H_0(n, m, k)$  are performed analytically and are given by

$$\begin{aligned} GA_0(n, k) &= \frac{1}{\epsilon_r + 1} \int_0^\infty \frac{J_{2n+1/2}(\xi) J_{2k+1/2}(\xi)}{\xi} d\xi \\ &= \frac{1}{\epsilon_r + 1} \frac{1}{4n+1} \delta_{nk} \end{aligned} \quad (14a)$$

$$\begin{aligned} H_0(n, m, k) &= \frac{1}{\epsilon_r + 1} \\ &\quad \cdot \int_0^\infty \frac{J_{2n+m+1/2}(\xi) J_{2k+1/2}(\xi) J_m(p\xi)}{\xi} d\xi \\ &= \frac{1}{\epsilon_r + 1} \frac{(-1)^{n+m}}{4n+2k+1} \sum_{l=0}^{\infty} \left\{ \frac{(2l+2n+2k+m+1)!}{l!(l+2n+2k+m+1)!} \right. \\ &\quad \left. \cdot \frac{\Gamma(l+n+k+m+\frac{1}{2}) \Gamma(l+n+k+\frac{1}{2})}{\Gamma(l+2n+m+\frac{3}{2}) \Gamma(l+2k+\frac{3}{2}) p^{2l+2n+2k+m}} \right\}. \end{aligned} \quad (14b)$$

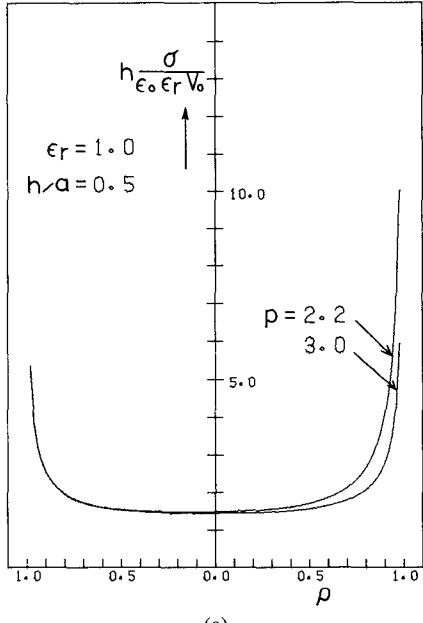


(a)

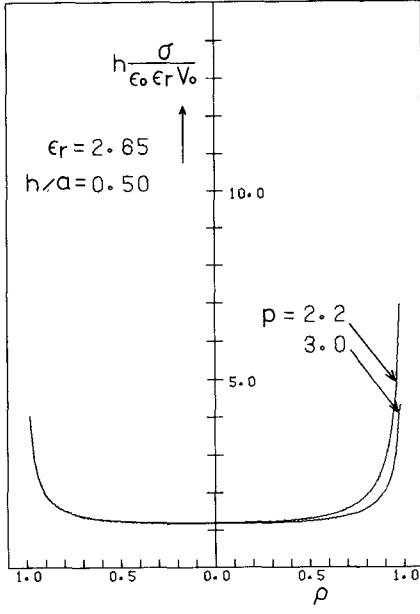


(b)

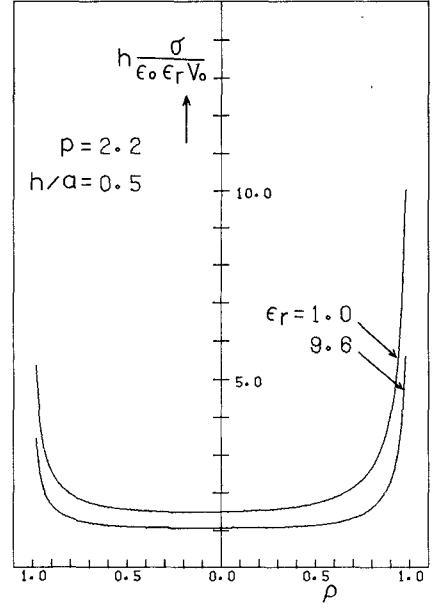
Fig. 2. The variation of expansion coefficients  $A_{mn}$  with respect to subscripts  $m$  and  $n$ . Thickness of the substrate is  $h/a = 0.5$  and separation between the disks is  $p = 2.2$ . (a)  $\epsilon_r = 1.0$ . (b)  $\epsilon_r = 9.6$ .



(a)



(b)



(c)

Fig. 3. The charge distribution on disk 1 in the presence of disk 2 when disk 1 and 2 are at potential  $V_0$  and  $-V_0$ , respectively.

The first integrals in (13) can be truncated by taking a finite range of integration, since the term  $P(\xi, h) - 1/(1 + \epsilon_r)$  decreases exponentially when the value of  $\xi$  increases. If the values of  $GA$  and  $H$  for various values of  $n$ ,  $k$ , and  $m$  are obtained, the determination of expansion coefficients  $A_{mn}$  is straightforward. A set of equations (6) is solved using a Gauss-Seidel procedure. It is worthwhile noting that the dependency of expansion coefficients  $A_{mn}$

on the subscripts  $m$  and  $n$ , where  $m$  and  $n$  refer to mode numbers along the circumferential and radial directions, respectively. In Fig. 2, we show the values of  $|A_{mn}|$  for various values of  $m$  and  $n$  when the relative dielectric constant of the substrate is  $\epsilon_r = 1.0$  (Fig. 2a) and  $\epsilon_r = 9.6$  (Fig. 2b), the thickness of the substrate is  $h/a = 0.5$ , and the separation between the disks is  $p = 2.2$ . In each case, the magnitude of  $A_{mn}$  decreases more rapidly with  $n$  than

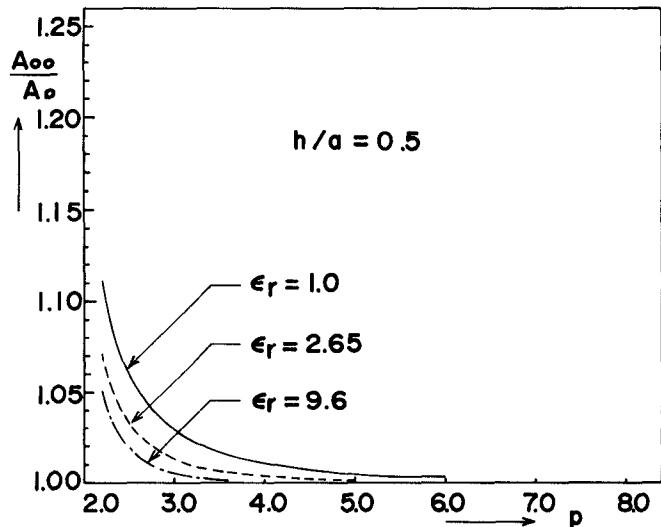


Fig. 4. The rate of increase of total charge distributed on disk 1 electrified to  $V_0$  due to the coupling with disk 2, which is at the potential  $-V_0$ .

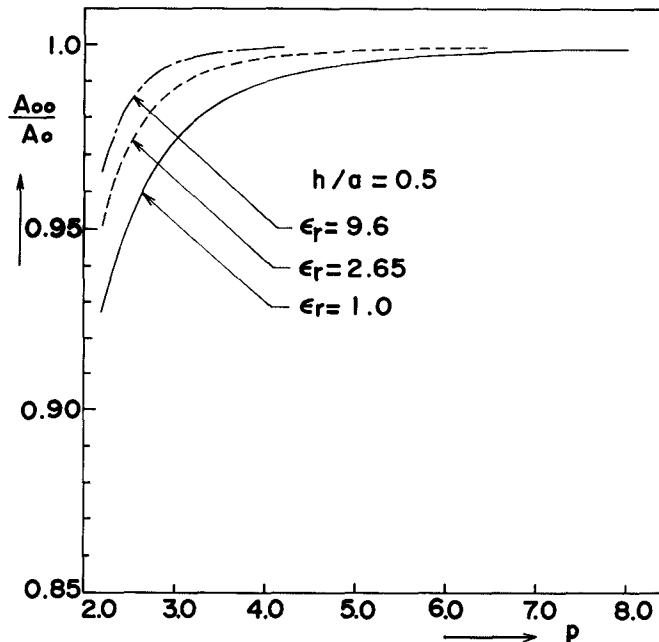


Fig. 5. The rate of decrease of total charge distributed on disk 1 electrified to  $V_0$  due to the coupling with disk 2, which is at the same potential.

with  $m$ . Experience shows that the number of modes along the circumferential direction ( $m$ ) should be roughly four times of that along the radial direction ( $n$ ) from the convergence point of view, particularly for tight coupling. But the choice was not so critical, and we have not experienced in this problem the phenomenon of relative convergence discussed in [13]. The numerical results for charge distribution on the disks are shown in Fig. 3, when disk 1 is at the potential of  $V_0$  and the disk 2 is at  $-V_0$ . These figures show the effects of thickness and dielectric constant of the substrate, and of the separation between the disks on the charge distribution on the disk. Each figure depicts the normalized charge distribution along the line connecting

the center of each disk.  $\rho = 1$  corresponds to the edge of the disk, and the charge density increases near the edge in a manner  $(1 - \rho^2)^{-1/2}$ . When the coupling is rather close, the charge density shows a tendency to concentrate around the edge close to another disk, and the symmetry of charge distribution is broken considerably. The degree of the asymmetry of the charge distribution is one of the measures of the amount of electrostatic coupling between the disks. When the dielectric constant of the substrate is very large or the thickness of the substrate is very small, the coupling effect is little recognized. Since the electric-field flux, which starts from disk 1 and ends on disk 2, increases as the disks come closer, the total charge stored in each

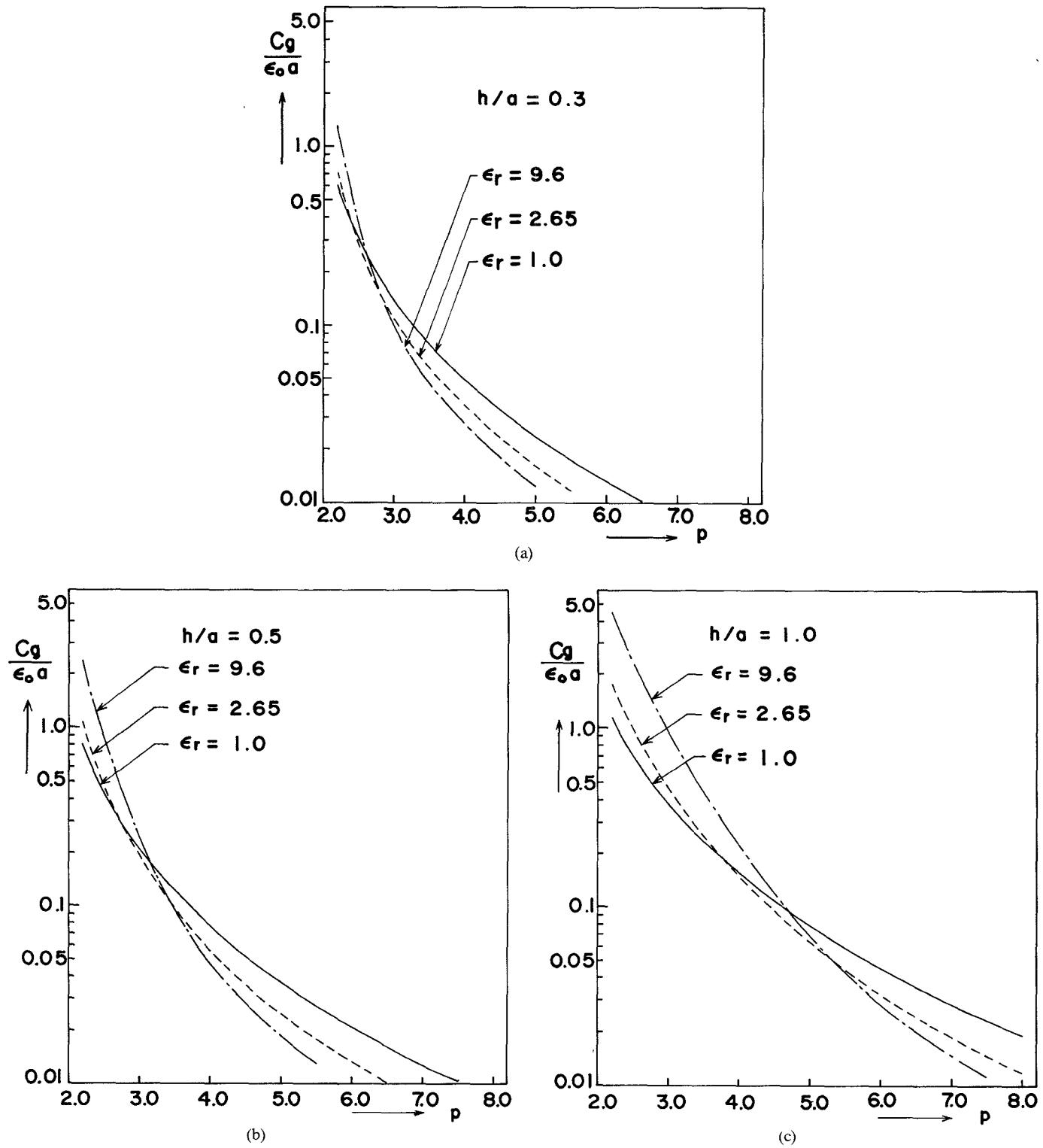


Fig. 6. The variation of gap capacitance  $C_g$  with respect to separation between disks  $p$ .

disk increases. As shown in (11), the total charge is proportional to the expansion coefficients  $A_0$ . The relations between the separation  $p$ , relative dielectric constant  $\epsilon_r$ , and  $A_{00}/A_0$  are shown in Fig. 4, where  $A_0$  is the corresponding expansion coefficient associated with a single disk. On the

other hand, when both disks are at the equal potential  $V_0$ , the total charge decreases to some limited values as the disks come closer. The behavior is shown in Fig. 5. Uzunoglu and Katechi proposed a gap capacitance  $C_g$  as a measure of electrostatic coupling between the disks, which

TABLE I  
POTENTIAL DISTRIBUTION ON THE SURFACE OF THE SUBSTRATE  
ALONG THE LINE JOINING THE CENTERS OF THE DISKS

t	POTENTIAL $\epsilon_r=1.0$	$\phi[v]$	$p=2.2$	$h/a=0.5$
1.1	0.000000	0.000000	0.000000	
1.0	0.998220	0.998161	0.998113	
0.75	0.999581	0.999583	0.999584	
0.5	0.999819	0.999743	0.999680	
0.25	1.001006	1.001101	1.001177	
0	1.001094	1.001300	1.001467	
-0.25	1.000209	1.000285	1.000347	
-0.5	0.999632	0.999556	0.999495	
-0.75	1.000068	1.000076	1.000083	
-1.0	0.999551	0.999500	0.999459	
-1.25	0.353900	0.306876	0.274874	
-1.5	0.195180	0.149021	0.118961	
-1.75	0.118062	0.079110	0.055030	
-2.0	0.075978	0.044892	0.026747	
-2.25	0.051301	0.027033	0.013693	
-2.5	0.036010	0.017179	0.007428	
-2.75	0.026095	0.011451	0.004292	

is defined as follows. Assuming the disks to be at the potential  $V_0$  and  $-V_0$ , the total charge on each disk will be

$$Q_D = 2C_g V_0 + Q_s \quad \text{or} \quad C_g = \frac{Q_D - Q_s}{2V_0}$$

where  $Q_s = CV_0$  is the total charge of single disk when it is raised to potential  $V_0$ .

The effects of separation between disks  $p$ , relative dielectric constant  $\epsilon_r$ , and thickness  $h$  of the substrate on the gap capacitance  $C_g$  are shown in Fig. 6. From these figures, gap capacitances  $C_g$  are found to decrease more rapidly with  $p$  when the permittivity of the substrate becomes larger. Finally, to check the validity of the present treatment, we calculated the potential distribution along the line joining each center of the disk when the disks are at the potential 1 V and -1 V. The results for  $p = 2.2$  and  $h/a = 0.5$  are shown in Table I, in which the potential is specified as 1 V in the range  $-1 < \rho/a < 1$ , as stated above, while the calculated values depart from specified value from 3 or 4 decimals at that range. The agreement improves with increasing  $p$ , though it is not shown here for saving space. The accuracy obtained here will be satisfactory for practical calculation.

#### IV. CONCLUSION

The coupling between the microstrip circular disks placed on a grounded dielectric substrate is studied analytically as an electrostatic potential problem. The problem is formulated using the Kobayashi potential and is reduced to a simultaneous equation for expansion coefficients. Some numerical results for physical quantities such as charge distribution, potential distribution, and gap capacitance are obtained. The obtained results will serve as a basis for practical design of microstrip circuit components or for criterion of newly developed analytical techniques for related problems.

#### APPENDIX

##### JACOBI'S POLYNOMIAL $u_n(x)$

Jacobi's polynomial  $u_n(x)$  used in this paper is defined by

$$\begin{aligned} u_n^m(x) &= \sqrt{\frac{2}{\pi}} x^{-m/2} \int_0^\infty \frac{J_m(\sqrt{x}\xi) J_{m+2n+1/2}(\xi)}{\sqrt{\xi}} d\xi \\ &= \frac{\Gamma(n+m+1/2)}{\sqrt{\pi} \Gamma(n+1) \Gamma(n+m+1)} x^{-m} (1-x)^{1/2} \frac{d^n}{dx^n} \\ &\quad \cdot \{x^{n+m} (1-x)^{n-1/2}\}. \end{aligned}$$

The bessel function  $J_m(p\sqrt{x})$  is expanded by the polynomial  $u_n^m(x)$  as

$$\begin{aligned} x^{-m/2} J_m(p\sqrt{x}) &= \sqrt{\frac{\pi}{2}} \sum_{n=0}^{\infty} (2m+4n+1) \\ &\quad \cdot \frac{J_{m+2n+1/2}(p)}{\sqrt{p}} u_n^m(x). \end{aligned}$$

The orthogonality relation for  $u_n^m(x)$  is given by

$$\begin{aligned} \left[ \int_0^1 x^m (1-x)^{-1/2} u_n^m(x) u_n^m(x) dx \right. \\ \left. = \frac{2\Gamma(n+\frac{1}{2})\Gamma(n+m+\frac{1}{2})}{\pi(2m+4n+1)\Gamma(n+1)\Gamma(n+m+1)} \delta_{nm} \right] \end{aligned}$$

#### REFERENCES

- [1] I. N. Sneddon. *Mixed Boundary Value Problems in Potential Theory*. New York: Wiley, 1966.
- [2] V. Hutson, "The circular plate condenser at small separations," in *Proc. Camb. Phil. Soc.*, vol. 59, 1963, pp. 211-224.
- [3] Y. Nomura, "The electrostatic problems of two equal parallel circular plates," in *Proc. Phys. Math. Soc. Japan*, vol. 3, no. 23, 1941, pp. 168-180.
- [4] F. Leppington and H. Levine, "On the capacity of the circular condenser at small separation," in *Proc. Camb. Phil. Soc.*, vol. 68, 1970, pp. 235-254.
- [5] S. R. Borkar and R. F. H. Yang, "Capacitance of a circular disk for application in microwave integrated circuits," *IEEE. Trans. Microwave Theory Tech.*, vol. MTT-23, pp. 588-591, 1975.
- [6] W. C. Chew and J. A. Kong, "Effects of fringing fields on the capacitance of circular microstrip disk," *IEEE. Trans. Microwave Theory Tech.*, vol. MTT-28, pp. 98-104, 1980.
- [7] I. Kobayashi, "Darstellung eines Potentials in zylindrischen Koordinaten, das sich auf einer Ebene innerhalb und ausserhalb einer gewissen Kreisbegrenzung verschiedener Grenzbedingung unterwirft," *Sci. Rep. Tohoku Imp. Univ.*, vol. XX, no. 2, 1931.
- [8] P. Benedek and P. Silvester, "Equivalent capacitances for microstrip gap and steps," *IEEE. Trans. Microwave Theory Tech.*, vol. MTT-20, pp. 729-733, 1972.
- [9] M. Maeda, "An analysis of gap in microstrip transmission lines," *IEEE. Trans. Microwave Theory Tech.*, vol. MTT-20, pp. 390-396, 1972.
- [10] I. Kobayashi, "Das elektrostatische Potential um zwei auf derselben Ebene liegende und sich nicht schneidende gleichgrosse Kreis Scheiben," *Sci. Rep. Tohoku Imp. Univ.*, vol. XXVII, no. 3, pp. 365-391, 1939.
- [11] N. K. Uzunoglu and P. Katechi, "Coupled microstrip disk resonators," *IEEE. Trans. Microwave Theory Tech.*, vol. MTT-28, pp. 94-97, 1980.
- [12] W. Magnus and F. Oberhettinger. *Formeln und Sätze für die Speziellen Funktionen der Mathematischen Physik*. Berlin: Springer-Verlag, 1948, p. 49.

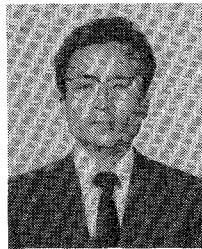
[13] R. Mittra and S. W. Lee. *Analytical Technique in the Theory of Guided Wave*. New York: MacMillan, 1971, pp. 36-41.

+



**Masaru Takahashi** was born in Kyoto, Japan, July 16, 1954. He received the B.E. and M.E. degrees from Shizuoka University, in 1980 and 1982, respectively.

In 1982 he joined the Technical Staff at Nippon Electric Co., working in development of the equipment associated with radio-wave propagation.



**Kohei Hongo** (S'62-M'62-M'75-SM'75) was born in Sendai, Japan, on June 2, 1939. He received the B.E., M.E., and D.E. degrees, all in electrical communication engineering, from Tohoku University, in 1962, 1964, and 1967, respectively. He was an Assistant at Tohoku University during 1967-1968.

Since 1968 he has been on the Faculty of the Department of Electrical Engineering in Shizuoka University, where he is currently a Professor. From 1974 to 1975 he was a visiting Associate Professor at the Department of Electrical Engineering, University of Illinois. His research interest is in the area of electromagnetic wave propagation and radiation.

Dr. Hongo is a member of the Institute of Electronics and Communication Engineers of Japan.

# Quasistatic Characteristics of Covered Coupled Microstrips on Anisotropic Substrates: Spectral and Variational Analysis

MANUEL HORNO, MEMBER, IEEE

**Abstract** — In this paper, expressions to compute the upper and lower bounds on true values of the even- and odd-mode capacitances of covered coupled microstrips over anisotropic substrates are obtained by using the Fourier transform and the variational approach. The method provides accurate calculation and yields the margins of error in the computation. Some examples are shown.

## I. INTRODUCTION

**I**N RECENT YEARS, the boundary value problems involving microstrip lines on anisotropic substrates have been approached from numerical [1] and analytical points of view [2]-[9]. Alexopoulos *et al.* [2], [3] have shown the effect of an anisotropic substrate on the characteristics of covered coupled microstrips by using the method of moments. Methods for calculating the parameters of single [4], [5] and coupled microstrip lines [6]-[8] have been performed by applying transformation from anisotropic to isotropic problems. Green's functions for examples with anisotropic medium have been obtained using the image-coefficient method in [9].

The spectral-domain approach has been used extensively on problems of microstrip lines on isotropic substrates, and variational expressions of capacitances have been reported [10], [11]. This method was extended by [12] and [13] to analyze the characteristic parameters of single and coupled microstrips on anisotropic substrates.

The purpose of this paper is to solve the variational problem involving covered coupled microstrips on anisotropic substrates with an arbitrary permittivity tensor by using the Fourier transform, and obtaining in this way stationary expressions to compute the upper and lower bounds of the mode quasi-static characteristics of this structure. The method shows the equivalence between the mode capacitances of this structure and another with an isotropic substrate, in agreement with the reported results [14]. Besides, it is a fast and accurate calculation method in most practical cases and it yields the margins of error in the computation.

## II. ANALYSIS

Consider the configuration of covered coupled microstrips shown in Fig. 1, which comprises two zero-thickness strips on an anisotropic dielectric substrate, which permit-

Manuscript received April 7, 1982; revised June 2, 1982.

The author is with the Departamento de Electricidad y Electrónica, Facultad de Física, Universidad de Sevilla, Seville, Spain.